


SET-A

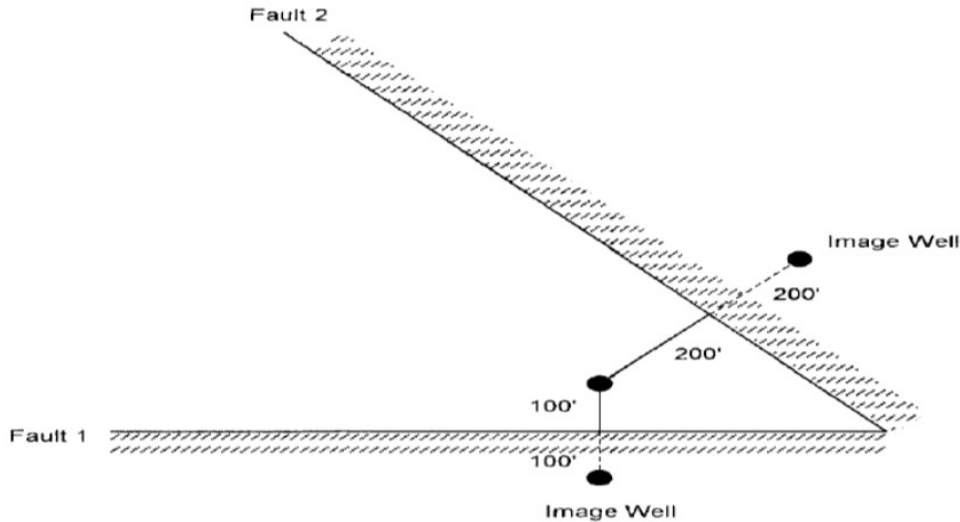
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| Name: |  UPES UNIVERSITY WITH A PURPOSE |
| Enrolment No: | |

UNIVERSITY OF PETROLEUM AND ENERGY STUDIES**End Semester Examination, May 2019****Course: Production Engineering and Well Testing & Analysis****Semester: IInd****Program: M.Tech (Petroleum Engineering)****Time 03 hrs.****Course Code: PEAU 7006****Max. Marks: 100****Instructions:** All the questions are compulsory.**SECTION A**

| S. No. | Questions | Marks | CO |
|--------|---|-------|-----|
| Q 1 | A 0.5 ft. diameter hole has a damaged region 4ft. deep. The permeability in this region is one tenth that of the undamaged region. Estimate skin effect and effective wellbore radii. | 4 | CO3 |
| Q 2 | Construct IPR curve for given problem: Given data: $\dot{P}_r = 2600$ psi; $P_{wf} = 1900$ psi; $q_o = 150$ bpd Find: $(q_o)_{max}$ and q_o for $P_{wf} = 1100$ psi | 4 | CO1 |
| Q 3 | Illustrate the causes of sand production. Write the methods for control sand production. | 4 | CO2 |
| Q 4 | Differentiate between carryover and blowby for the storage of oil and gas. | 4 | CO2 |
| Q 5 | Illustrate how a typical Drill Stem Test is performed. Prepare and examine a schematic chart of pressure vs. time from a test with two flow periods and two shut in periods. | 4 | CO4 |

SECTION B

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|-----|--|-----------|------------|
| Q 6 | Figure shows a well located between two sealing faults at 200 and 100 feet from the two faults. The well is producing under a transient flow condition at a constant flow rate of 200 STB/day. The following additional data is available: $B = 1.1$ bbl/STB; $\mu = 2.0$ cp; $r_w = 3.0$ ft; $C_t = 25 \times 10^{-6}$ psi ⁻¹ ; $k = 60$ md; $\Phi = 17\%$; $h = 25$ ft; $P_i = 5000$ psi; $E_i(0.537) = 0.514$; $E_i(2.15) = 0.0476$. Calculate the sand face pressure after 10 hours. | 10 | CO3 |
|-----|--|-----------|------------|



Q 7 A new oil well with an infinite acting boundary produced 500 STB/D for 3 days, it then was shut in for a pressure buildup test, during which the following data were recorded. If the wellbore radius, r_w is 0.3 ft; net sand thickness, h is 22 ft; formation volume factor, B_o is 1.3 RB/STB; porosity, ϕ is 0.2; total compressibility, C_t is 20×10^{-6} psi⁻¹; and oil viscosity, μ_o is 1.0 cp. estimate Formation Permeability and Skin Factor.

| | | | | | | | |
|---------------------------------|------|------|------|------|------|------|------|
| Shut-in Time, Δt (hrs.) | 0 | 2 | 4 | 8 | 16 | 24 | 48 |
| P_{ws} (psig) | 1150 | 1794 | 1823 | 1850 | 1876 | 1890 | 1910 |

10 CO4

Q 8 What are the parameters affecting the separation process of oil and gas. Describe the working procedure of vertical heater-treater with suitable diagram.

10 CO2

Q 9 Estimate the oil permeability, skin factor and additional pressure drop due to the skin from the following drawdown data: $h = 130$ ft., $\phi = 20\%$, $r_w = 0.25$ ft., $p_i = 1154$ psi, $q_o = 348$ stb/d, $m = -22$ psi/cycle, $B_o = 1.14$ bbl/STB, $\mu_o = 3.93$ cp, $C_t = 8.74 \times 10^{-6}$ psi⁻¹, $p_{1hr} = 954$ psi. Assuming that the wellbore storage effect is not significant.

10 CO5

OR

Using Fetkovich's equation plot the IPR curve for a well in which P_i is 2500 psia and J'_i is 5×10^{-4} stb/day-psi². Predict the IPRs of the well at well shut in static pressures of 2000 and 1500 psia.

CO1

SECTION-C

Q 10 Predict the operating point to use an artificial lift in the gas well with the help of Nodal analysis graph. Data are given below:
 Gas specific gravity (γ_g) = 0.71, tubing inside diameter (D) = 2.259 in., tubing relative roughness (e/D) = 0.0006, Measured depth at tubing shoe (L) = 10000 ft., Inclination angle (θ) = 0 degrees, Wellhead pressure (p_{hr}) = 800 psia, Wellhead temperature (T_{hr}) = 150 °F, Bottom-hole Temperature (T_{wf}) = 200 °F, Reservoir Pressure = 2000 psia, C-constant in back pressure IPR model = 0.01 Mscf/d-psi²ⁿ, n-exponent in back pressure IPR model = 0.8, Avg. temperature (T_{av}) = 635 °R, compressibility factor (Z_{av}) = 0.8626, skin factor (s) = 0.4861, moody friction factor (f_m) = 0.0174, absolute open flow (AOF) = 1912.705 Mscf/d.

20 CO1

Q 11

Explain Ramey’s type curve, Mckinley’s type curve and Gringarten et al. type curve. Also write the uses of these type curves.

OR


A constant-rate pressure drawdown test was run in a well with the following characteristics:

$q = 250$ STB/D (constant); $\Phi = 0.039$; $\mu = 0.8$ cp; $C_t = 17 \times 10^{-6}$ psi⁻¹; $r_w = 0.198$ ft; $h = 69$ ft; $B_o = 1.136$ RB/STB; $A_{wb} = 0.0218$ sq ft; $\rho = 53$ lb/cu ft. From the test data in the following table, estimate formation permeability, skin factor, Liquid/gas interface and wellbore storage duration.

| t, hrs | P_{wf} psia | t, hrs | P_{wf} psia | t, hrs | P_{wf} psia | t, hrs | P_{wf} psia |
|---------------|---------------------------------|---------------|---------------------------------|---------------|---------------------------------|---------------|---------------------------------|
| 0 | 3000 | 0.164 | 2693 | 3.28 | 1712 | 38.2 | 1533 |
| 0.0109 | 2976 | 0.218 | 2611 | 3.82 | 1696 | 43.7 | 1525 |
| 0.0164 | 2964 | 0.273 | 2536 | 4.37 | 1684 | 49.1 | 1517 |
| 0.0218 | 2953 | 0.328 | 2469 | 4.91 | 1674 | 54.6 | 1511 |
| 0.0273 | 2942 | 0.437 | 2352 | 5.46 | 1665 | 65.5 | 1500 |
| 0.0328 | 2930 | 0.491 | 2302 | 6.55 | 1651 | 87.4 | 1482 |
| 0.0382 | 2919 | 0.546 | 2256 | 8.74 | 1630 | 109.2 | 1468 |
| 0.0437 | 2908 | 1.09 | 1952 | 10.9 | 1587 | 163.8 | 1440 |
| 0.0491 | 2897 | 1.64 | 1828 | 16.4 | 1568 | 218.4 | 1416 |
| 0.0546 | 2886 | 2.18 | 1768 | 27.3 | 1554 | 273.0 | 1393 |
| 0.109 | 2785 | 2.73 | 1734 | 32.8 | 1543 | 327.6 | 1370 |

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CO5

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UNIVERSITY OF PETROLEUM AND ENERGY STUDIES

End Semester Examination, May 2019

Course: Production Engineering and Well Testing & Analysis

Semester: IInd

Program: M.Tech (Petroleum Engineering)

Time 03 hrs.

Course Code: PEAU 7006

Max. Marks: 100

Instructions: All the questions are compulsory.

SECTION A

| S. No. | Questions | Marks | CO |
|--------|--|-------|-----|
| Q 1 | Explain the procedure of Drill Stem Test. Prepare and examine a schematic chart of pressure vs. time from a test with two flow periods and two shut in periods. | 4 | CO4 |
| Q 2 | In a well test analysis by Ramey's Type curve, a "match point" is obtained from the actual graph of log (ΔP) vs log t and Ramey's type curve of log P_D vs log t_D . Corresponding to the "match point" following data are obtained: $(\Delta P)_{MP} = 100$ psig, $(P_D)_{MP} = 0.85$, $(t)_{MP} = 1$ and $(t_D)_{MP} = 1.93 \times 10^4$. Other reservoir properties are: OFVF (B_o) = 1.2 bbl/STB, viscosity (μ_o) = 0.8 cp, total compressibility (c_t) = 10×10^{-6} psi ⁻¹ , thickness (h) = 56 ft, initial reservoir pressure (p_i) = 3000 psi, flow rate (q) = 500 STB/day and wellbore radius (r_w) = 0.3 ft Calculate the permeability and porosity of the reservoir $P_D = \frac{0.00708 kh (P_i - P_{wf})}{q\mu B_o} \wedge t_D = \frac{0.0002637 kt}{\phi \mu C_t r_w^2}$ | 4 | CO3 |
| Q 3 | What are the well stimulation jobs applicable to enhanced oil production and why do we need to perform well stimulation jobs? | 4 | CO2 |
| Q 4 | Classify the separators used in oil industry. What are parameters affects the separation process during oil and gas separation? | 4 | CO2 |
| Q 5 | A 12 inch diameter hole has a stimulated region 48 inch deep. The permeability in this region is one tenth that of the undamaged region. Estimate skin effect and effective wellbore radii. | 4 | CO3 |

SECTION B

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|---------------------------------|--|---------------------------------|------|------|------|------|------|----|----|-----------------|------|------|------|------|------|------|------|-----------|------------|
| Q 6 | <p>A new oil well with an infinite acting boundary produced 800 STB/D for 3 days, it then was shut in for a pressure buildup test, during which the following data were recorded. If the wellbore radius, r_w is 0.3 ft; net sand thickness, h is 22 ft; formation volume factor, B_o is 1.3 RB/STB; porosity, ϕ is 0.2; total compressibility, C_t is 20×10^{-6}psi⁻¹; and oil viscosity, μ_o is 1.0 cp. estimate Formation Permeability and Skin Factor.</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 15%;">Shut-in Time, Δt (hrs.)</td> <td style="width: 10%;">0</td> <td style="width: 10%;">2</td> <td style="width: 10%;">4</td> <td style="width: 10%;">8</td> <td style="width: 10%;">16</td> <td style="width: 10%;">24</td> <td style="width: 10%;">48</td> </tr> <tr> <td>P_{ws} (psig)</td> <td>1150</td> <td>1794</td> <td>1823</td> <td>1850</td> <td>1876</td> <td>1890</td> <td>1910</td> </tr> </table> | Shut-in Time, Δt (hrs.) | 0 | 2 | 4 | 8 | 16 | 24 | 48 | P_{ws} (psig) | 1150 | 1794 | 1823 | 1850 | 1876 | 1890 | 1910 | 10 | CO4 |
| Shut-in Time, Δt (hrs.) | 0 | 2 | 4 | 8 | 16 | 24 | 48 | | | | | | | | | | | | |
| P_{ws} (psig) | 1150 | 1794 | 1823 | 1850 | 1876 | 1890 | 1910 | | | | | | | | | | | | |

| Q 7 | <p>Predict future IPR curves for given problem.</p> <p>Given data: 45 - acre spacing. Residual oil saturation = 16% $J = 0.90$. Interstitial water saturation = 21% $q = 500$ bpd $P_r = 2500$ psig</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 30%;">Parameters</th> <th style="width: 35%;">Present</th> <th style="width: 35%;">Future</th> </tr> </thead> <tbody> <tr> <td>P_r</td> <td>2500 psig</td> <td>2100 psig</td> </tr> <tr> <td>P_{wf}</td> <td>1200 psig</td> <td>1200 psig</td> </tr> </tbody> </table> | Parameters | Present | Future | P_r | 2500 psig | 2100 psig | P_{wf} | 1200 psig | 1200 psig | 10 | CO1 |
|------------------|--|------------|--------------------|--------|-------|-----------|-----------|----------|-----------|-----------|-----------|------------|
| Parameters | Present | Future | | | | | | | | | | |
| P_r | 2500 psig | 2100 psig | | | | | | | | | | |
| P_{wf} | 1200 psig | 1200 psig | | | | | | | | | | |
| Q 8 | <p>Differentiate between carryover and gas for the storage and gas. Describe the working procedure of horizontal well greater with suitable diagram.</p> | 10 | CO2 | | | | | | | | | |
| Q 9 | <p>A constant rate drawdown test was run in a well with following characteristics: wellbore radius (r_w) = 0.198 ft, total compressibility (c_t) = 17×10^{-6} psi⁻¹, Oil compressibility (c_o) = 10×10^{-6} psi⁻¹, production rate (q_o) = 250 STB/D, thickness (h) = 69 ft, viscosity (μ_o) = 0.8 cp, porosity (ϕ) = 0.039, OFVF (B_o) = 1.136 bbl/STB, initial reservoir pressure P_i = 4412 psia. The Annulus cross-sectional area is 0.0218 sq ft, the density of the fluid in the wellbore is 53 lbm/cu ft and volume of the fluid in wellbore is 200 bbl. The wellbore has falling liquid/gas interface.</p> <p>Following data are obtained from semi-logarithmic plot of flowing BHP (P_{wf}) vs time (t): Slope of middle time region (MTR) = 70 psi/cycle and pressure at one hour (P_{1h}) = 3652 psia.</p> <p>Calculate: (i) Formation permeability (ii) Skin factor (iii) Pressure drop due to skin (iv) Time to end wellbore storage effect</p> $t_{wbs} = \frac{(200000 + 12000 s) C_s}{\frac{kh}{\mu}}, \text{ where } C_s \text{ is wellbore storage constant}$ <p style="text-align: center;">OR</p> <p>A 1640 ft long horizontal well is drilled in the lowest zone of an oil reservoir. The reservoir has a gas cap. Calculate critical oil production rates for horizontal and vertical wells using Joshi Method. The well is placed at 160 acres well spacing. The vertical well is perforated in the bottom 8 ft. to minimize gas coning.</p> <p>The following data are given: $K_h = k_v = 70$ md, $h = 80$ ft., $2X_e = 2640$ ft., $B_o = 1.1$ RB/STB, $\mu_o = 0.42$ cp, $r_w = 0.328$ ft., $\rho_o - \rho_g = 0.48$ gm/cc, $h_p = 8$ ft. for vertical wells.</p> | 10 | CO5 CO1 | | | | | | | | | |
| SECTION-C | | | | | | | | | | | | |
| Q 10 | <p>Explain Ramey's type curve, McKinley's type curve and Gringarten et al. type curve. Also write the uses of these type curves.</p> | 20 | CO5 | | | | | | | | | |
| Q 11 | <p>Derive an expression for determining future IPR with the help of Fetkovich's method with proper assumptions. Using Fetkovich's method, plot the IPR curve for a well in which P_i is 3000 psia and $J_o^i = 4 \times 10^{-4}$ stb/day-psia². Predict the IPRs of the well at well shut in static pressures of 2500 psia, 2000 psia, 1500 psia and 1000 psia.</p> <p style="text-align: center;">OR</p> <p>Predict the operating point to use an artificial lift in the gas well with the help of Nodal analysis graph. Data are given below: Gas specific gravity (γ_g) = 0.71, tubing inside diameter (D) = 2.259 in., tubing relative roughness (e/D) = 0.0006, Measured depth at tubing shoe (L) = 10000 ft., Inclination angle (θ) = 0 degrees, Wellhead pressure (p_{hf}) = 800 psia, Wellhead</p> | 20 | CO1 | | | | | | | | | |

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|---|--|--|
| temperature (T_{hf}) = 150 °F, Bottom-hole Temperature (T_{wf}) = 200 °F, Reservoir Pressure = 2000 psia, C-constant in back pressure IPR model = 0.01 Mscf/d-psi ²ⁿ , n-exponent in back pressure IPR model = 0.8, Avg. temperature (T_{av}) = 635 °R, avg. compressibility factor (Z_{av}) = 0.8626, skin factor (s) = 0.4861, moody friction factor (f_m) = 0.0174, absolute open flow (AOF) = 1912.705 Mscf/d. | | |
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